



Clinical assessment of intraocular pressure: a whole-eye dynamic model

Francesca Stefanoni¹, Alon Harris³, Marcela Szopos², Christophe Prud'homme², Riccardo Sacco¹, Dario Messenio⁴, Maria Laura Costantino¹, Giovanna Guidoboni²

¹Department of Mathematics, Politecnico di Milano (Polytechnic University of Milan), Milan, Italy; ²Institute for Advanced Mathematical Research, UMR 7501, National Center for Scientific Research, University of Strasbourg, Strasbourg, France; ³Eugene and Marilyn Glick Eye Institute, Indiana University School of Medicine, Indianapolis, IN, USA; ⁴Eye Clinic, Department of Clinical Science - ASST Fatebenefratelli Sacco, University of Milan, Milan, Italy

Abstract

The aim of this work is to provide a quantitative description of how geometrical and material properties of ocular tissues and fluids influence intraocular pressure (IOP).

Keywords: intraocular pressure (IOP), glaucoma management, mathematical modeling, sensitivity analysis

1. Introduction

IOP assessment is a simple, quick and non-invasive test that can be performed in any ophthalmology clinic. IOP alterations are associated with many diseases, such as glaucoma, and it is therefore of great clinical interest to identify the factors influencing IOP levels. Indeed, it is well known that geometrical and material properties characterizing ocular tissues and fluids influence IOP. In this context, the main goal of this work is to address the need for quantitative understanding of the influence of patient-specific geometrical and material properties of ocular tissues and fluids on IOP by means of mathematical modeling.

Correspondence: Francesca Stefanoni, Department of Mathematics, Politecnico di Milano, via Bonardi 9, Milano, Edificio 14 "La Nave" Campus Leonardo del Politecnico di Milano, Milan, Italy.

E-mail: Francesca.stefanoni91@gmail.com

2. Methods and results

The model aims to be an electrical analog of the physiology of the eye, including various details regarding structural mechanics and fluid dynamics. Interestingly, pressure values inside the eye exhibit a static component, mainly due to the balance of aqueous humor (AH) inflow and outflow, and a dynamic component, mainly due to blood flow oscillations. We considered both static and dynamic components, and in particular, we investigated and quantified the influence of tissue (vitreous humor, cornea, and sclera) deformability and blood flow pulsatility on the dynamic measurements of IOP. Model calibration and validation have been performed using published data. The model has been implemented using the open access software OpenModelica (Open Source Modelica Consortium: Linköping, Sweden) in order to facilitate further model extensions and connections with other models already available for different parts of the eye.

2.1. Basic modeling assumptions

We defined the total volume of the eye as the sum of volumes of aqueous humor (anterior chamber), choroidal blood, and internal structures (vitreous humor, lens, and iris):

$$V_{tot} = V_{AH} + V_{blood} + V_{struc} \quad (1)$$

In our model, the analog of volume is the electrical charge, whereas the analog of volumetric flow rate is the electrical current. In the following sections, we review three models that simulate IOP under different assumptions. The models can be thought of as successive steps towards the modeling of whole-eye dynamics.

2.2. Static conditions

As a first step, pressure is assumed to be uniform inside the eye, while choroid and structure volumes are assumed to be given constants. The steady-state value of IOP is computed as the solution of the equation that describes the balance between AH production and drainage, as in Szopos *et al.*:¹

$$\frac{dV_{AH}}{dt} = J_{in} - J_{out} = 0 \quad (2)$$

AH inflow is due to the processes of ultrafiltration and ionic secretion, whereas the outflow occurs through the trabecular and uveoscleral pathways. The balance leads to a scalar third order polynomial equation in the sole unknown IOP:

$$L[(cBP - IOP) - \sigma_p \Delta \pi_p - \sigma_s \Delta \pi_s] = \frac{1}{R_0[1 + Q(IOP - EVP)]} (IOP - EVP) + \frac{k_1}{k_2 + IOP} IOP \quad (3)$$

Using published data for the parameters (see Table 1), the value for the steady-state

Table 1. Control state values for the parameters

Parameter	Value and Unit	Meaning
L	0.3 $\mu\text{l}/\text{min}/\text{mmHg}$	hydraulic conductance
cBP	27.5 mmHg	ciliary blood pressure
$\Delta\pi_p$	25 mmHg	oncotic pressure difference
σ_p	1 [-]	protein reflection coefficient
$\Delta\pi_s$	-450 mmHg	osmotic pressure difference
σ_s	0.0515 [-]	low-molecular component coefficient
EVP	8 mmHg	episcleral vein pressure
R_o	2.2 mmHg min/ μl	resistance when pressure gradient equals zero
Q	0.012 mmHg	outflow obstruction coefficient
k_1	0.4 $\mu\text{l}/\text{min}$	maximum uveoscleral flow rate
k_2	5 mmHg	pressure corresponding to half max uveoscleral flow rate

Baseline values for the parameters: typical conditions of a healthy eye.

IOP found by OpenModelica is 14.9527 V, which is perfectly in the range of physiological IOP measured in the clinics. We performed a deterministic sensitivity analysis on Equation (3) showing that the major influence on IOP is given by $\Delta\pi_p$, $\Delta\pi_s$, and cBP, as shown in Figure 1.

2.3. Dynamic conditions

2.3.1. Ocular hemodynamics

We introduced a non-stationary component in the model starting from the model presented in Kiel *et al.*² The new assumption with respect to the previous model is that IOP depends on V_{tot} as in Equation (4), the given functions of time, $V_{ch}(t)$, and its first derivative, $G_{ch}(t)$, estimated as in Krakau.³ The new model is thus described by the following system of equations:

$$\left\{ \begin{array}{l} \frac{dV_{tot}}{dt} = J_{in} - J_{out} + G_{ch} \\ \overline{IOP} = \overline{IOP} 10^{\gamma(V_{tot} - \overline{V_{tot}})} \end{array} \right. \quad (4)$$

where γ is a constant equal to 0.0215 μl^{-1} and overlined variables indicate baseline values according to literature (15 mmHg and 7 ml, respectively, for \overline{IOP} and $\overline{V_{tot}}$). Changes in choroidal volume due to blood flow variations, namely $G_{ch}(t)$, are given by a sinusoidal current source. Changes in total volume, namely dV_{tot}/dt , are modeled by a capacitor, accounting for energy storage due to structural deforma-

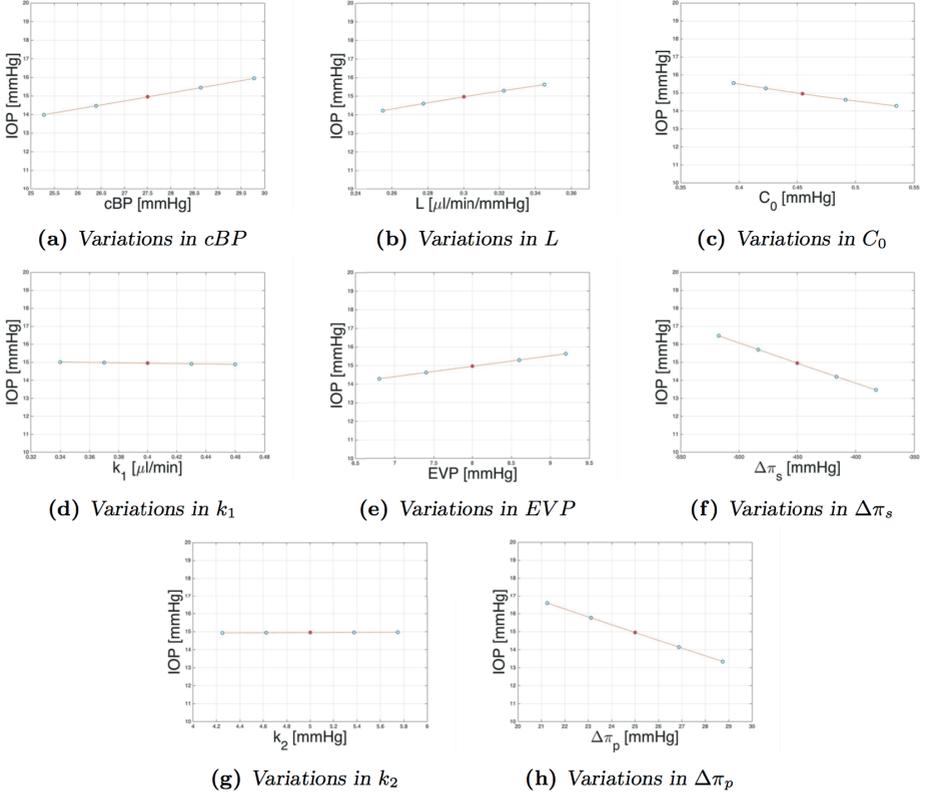


Fig. 1. Influence of different factors on IOP. Red dots indicate control state values for the variables and IOP; blue dots indicate samples used in the circuit.

bility of the eye. For the calibration of the current generator, we chose a frequency equal to the one of the clinically-measurable IOP wave, namely $1.1\bar{3} S^{-1}$. Oscillations in IOP indeed reflect changes in eye volume due to changes in the intraocular blood volume induced by the arterial blood pulse; thus, this frequency is that of the cardiac cycle. The amplitude value has been chosen to be $10.3166 \mu\text{L} S^{-1}$, as in Krakau.³

2.3.2. Ocular deformability

As a first step, we estimated a constant value for the capacity by means of a linearization of the relationship between IOP and V_{tot} shown in Equation (4):

$$C = \frac{\Delta V_{tot}}{\Delta IOP} = \frac{1}{\sqrt{IOP}} = 1.35 \mu\text{l mmHg}^{-1} \quad (5)$$

Note that γ in Equation (5) is the same as in Equation (4), but with the relation expressed in natural logarithm. γ accounts for the elastic properties of the cornea,

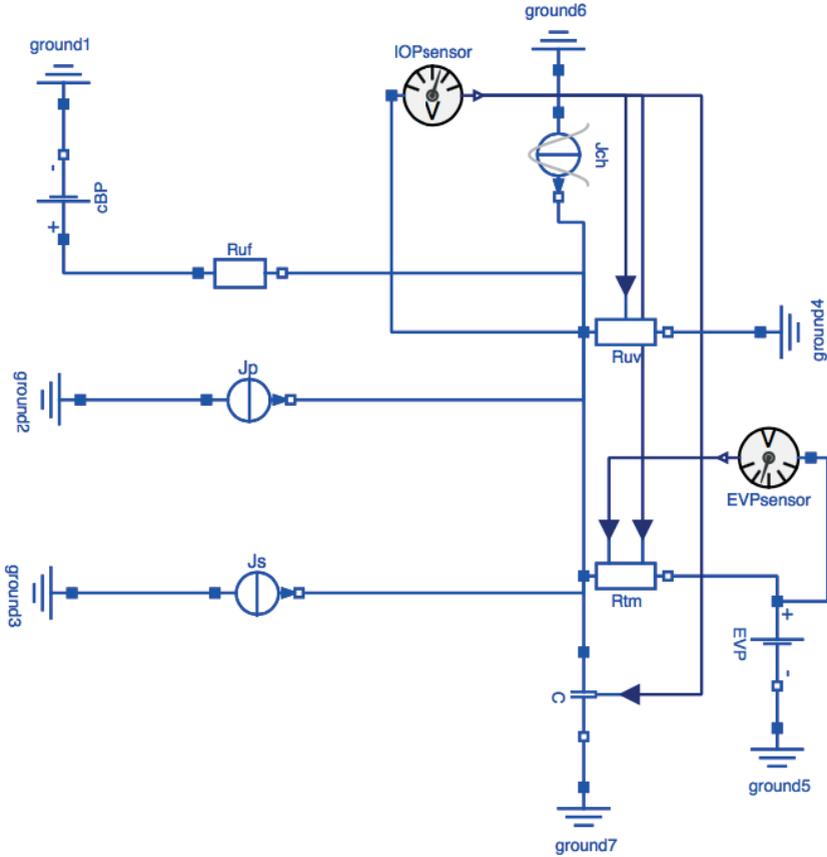


Fig. 2. OpenModelica electrical circuit for the dynamic component of IOP.

sclera, and other boundary structures of the eye, and is named ocular rigidity as in Friedenwald.⁴

Then we estimated a more precise non-linear value of the capacity as a function of IOP:

$$C = \frac{1/2 \log\left(\frac{IOP}{IOP_0}\right)}{IOP - IOP_0} \quad (6)$$

The circuit implemented in OpenModelica and the resultant IOP wave are shown in Figures 2 and 3, respectively. The sinusoidal IOP has an average value of 15.0179 mmHg and a range of variability of ± 2.12 mmHg, both increased with respect to the results found with the constant capacitance.

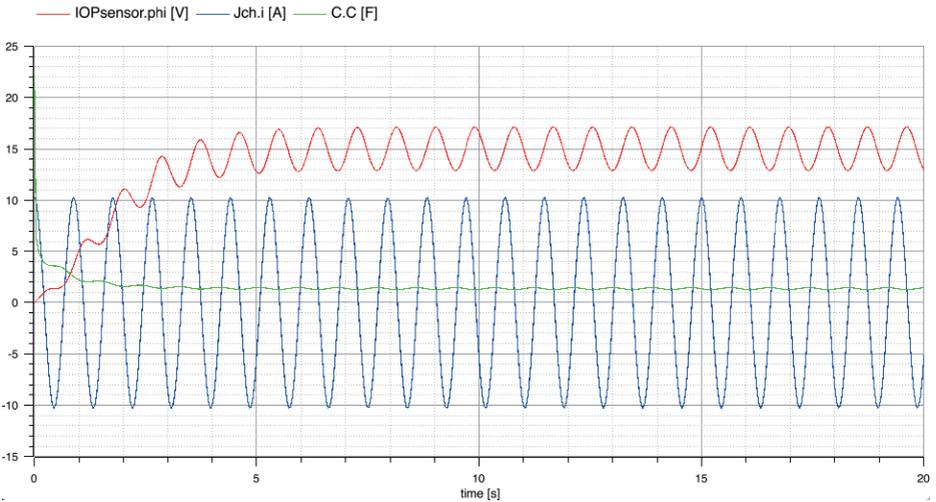


Fig. 3. OpenModelica simulation output: IOP, current generator Jch, and capacitor C.

3. Conclusions

This project provides a first attempt to consistently combine the static and dynamic components contributing to the pressure distribution inside the eye. It will help elucidate the relationship between the measured values of IOP and some important factors that may vary among patients. In a long-term perspective, the software developed within this project will be integrated within a larger virtual simulator for ocular biophysics, which may lead to a new tool for clinical use aimed at providing physicians with an integrated view of the patient's status to monitor, prevent, and treat diseases in a patient-specific manner.

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